## User Guide \#0601

## IRDC2086-330W Reference Design

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## Overview

The IRDC2086-330W Reference Design is a 330W, 97\% efficient, 48V-to-9.6V (35A), unregulated full bridge DC bus converter. The featured chipset solution consists of the IR2086S control IC, 80V primary side DirectFETs (IRF6646), 30V secondary side DirectFETs (IRF6635), primary side biasing FET (IRF7380) and the secondary side gate clamp FET (IRF6621).

The DC bus converter, with 50\% duty ratio offers the following features:

1. Zero voltage switching (ZVS) of the primary switches. This feature also guarantees the flux balance of the transformer.
2. The reverse recovery of the secondary synchronous FETs is eliminated due to the soft turn off of the secondary switch. The voltage stress of the secondary switch is also minimized.
3. The effective duty ratio is increased due to the ZVS operation. Loss associated with the dead-time is reduced. The ripple of the output current and the core loss of the output inductor are also reduced.

## Board Description and Circuit Capability



Fig. 1. The pictures of DC bus converter demo board with IR2086S Chipset: (a) front side and (b) back side of the converter.

The IR2086-330W is an open-loop, isolated full-bridge DC-DC converter with 5:1 voltage conversion ratio. The front side and back side of the demo board are shown in Fig. 1.

To evaluate operation and performance, connect a power supply to the input terminals and a power load to the output terminals. Input and output terminals are marked in Fig. 1. To duplicate the performance data reported on page two, approximately 400 LFM of airflow is needed across the module.
The circuit is designed to deliver continuous 30 A output current in the $40 \mathrm{~V}-60 \mathrm{~V}$ input voltage range, with 400 LFM of airflow. Output voltage for this input voltage range will vary from 7.7 V to 12.0 V , and the total available output power from the module will range from around 300 W at 40 V to about 350 W at 60 V input. The complete schematic of the demo board is shown in Fig. 2.

Fig. 2. Board Schematic


To optimize the performance with wide input voltage range, the converter is operated with variable frequency. The variable switching frequency is realized by connecting the timing resistor R15 to $\mathrm{V}_{\text {in }}$ via a zener diode D (the footprint is labeled as R14 on the PCB board). When the $\mathrm{V}_{\text {in }}$ is low, the charge current for the timing capacitor C 10 is low. Therefore, a low switching frequency is generated. The range of the switching frequency is 133 kHz to 226 kHz when the input voltage varies from 40 to 60 V . Curve 1 in Fig. 3 shows the switching frequency variation vs. the input voltage. The benefit of the variable frequency is the reduction of the losses due to the reduced magnetizing current when the input voltage increases, as observed from curve 2.

Fixed operation frequency can be achieved easily by removing $D(R 14)$ and connect the timing resistor R11 to $\mathrm{V}_{\mathrm{cc}}$. Fixed operation frequency is a good option when the input voltage is narrow. Curve 3 in Fig. 3 shows the magnetizing current variation when the converter is operated with a constant 180 kHz switching frequency.


Fig. 3. Magnetizing current with constant and variable frequency.
The circuit starts to operate when the primary voltage reaches about 32 V , sending pin 1 of the voltage detector (U2) high. The gate of the Q5 is about $14 \mathrm{~V} . \mathrm{V}_{\mathrm{cc}}$ is generated and the circuit begins to operate. After that, the high frequency voltage filtered by D5 sustains $\mathrm{V}_{\mathrm{cc}}$.

The circuit design is size-optimized in order to demonstrate true performance of the IR2086S control IC, IRF6646 primary FETs and IRF6635 secondary FETs. To probe the circuit waveforms use an oscilloscope probe with minimal length for the ground pin and connect directly to the pins of the IC/MOSFET device.

To measure circuit efficiency, the voltage and current at the input and output of the demo board need to be accurately measured. Use of calibrated shunts for input and output current measurements is strongly recommended, as is use of a thermal camera for thermal performance evaluation. Efficiency measurements at $\mathrm{V}_{\text {in }}=48 \mathrm{~V}$ and different output power are shown in Fig. 4. The black curve shows the efficiency with two IRF6635 in each secondary socket (total four IRF6635) with an output power to $P_{0}=325 \mathrm{~W}\left(V_{0}=9.3 \mathrm{~V}, I_{0}=35 \mathrm{~A}\right)$. The gray curve shows the efficiency measurements with one IRF6635 in each secondary socket with output power to $P_{0}=325 \mathrm{~W}$.


Fig. 4. Efficiency at 48-60Vin, 350W max with 400LFM air flow.

Thermal images with 325W output power at 48Vin with four IRF6635 and two IRF6635 are shown in Fig. 5(a) and (b) respectively. Temperature measurements at different conditions are listed in table 1. Inputs and outputs of two or more modules can be connected in parallel to provide required higher output power. Due to natural output voltage droop associated with open-loop operation, no additional circuitry is required for accurate current sharing (+/-10\%).


Fig. 5. Thermal image at $48 \mathrm{Vin}, 325 \mathrm{~W}$ output power with 400 LFM air flow:

Table 1. Temperature measurement $\left({ }^{\circ} \mathrm{C}\right)$ at $\mathrm{V}_{\text {in }}=48 \mathrm{~V}$ and $\mathrm{I}_{0}=35 \mathrm{~A}$.

|  | IRF6646 |  | IRF6635 |  | IR2086S | Transformer | Driver | Inductor |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| IRF6635 $\times 4$ | 66 | 71 | 70 | 71 | 69 | 62 | 66 | 49 |
| IRF6635 $\times 2$ | 73 | 76 | 78 | 80 | 74 | 67 | 72 | 53 |

As shown in Fig. 2, the primary side current is sensed with a current transformer. The current transformer turns ratio is 150:1. The sensed AC current information is rectified and fed into the current sense pin of the IR2086S after some RC filtering. Fig. 6 shows the output voltage during current hiccup mode. Current limit was set at 42A and the load was increased over the current trip point. It can be seen that the controller attempts to turn on the converter once in a period of 400 ms . The 400 ms period is determined by the external capacitance of C9.


Fig. 6. Output voltage waveform during hiccup mode at current limit setting of 42A.
During remote shut down, CR10 provides a path to discharge the bias stored in C16 quickly.

International I $\theta R$ Rectifier

## Layout

Fig. 7. Board PCB Layout (Total of 12 layers). Gerber files available on request.

| (a) top Layer | (b) bottom layer |
| :---: | :---: |
| (c) layer 1 | (d) layer 2 |
| (e) layer 3 | (f) layer 4 |
| (g) layer 5 | (h) layer 6 |
| (i) layer 7 | (j) layer 8 |
| (k) layer 9 | (I) layer 10 |

Bill Of Material (BOM)

|  | Designator | Category | Part Type | Footprint | Part Number | Vendor |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | C16, C9 | Capacitors | 0.1 u 50 V | 0603 SMD | PCC2153CT | Digi-Key |
| 2 | C10 | Capacitors | 220p, 50V | 0603 SMD | PCC221BVCT | Digi-Key |
| 3 | C1, C15 | Capacitors | 10000pF, 50V | 0603 SMD | 490-1512-1-ND | Digi-Key |
| 4 | C11, C12, C14 | Capacitors | 33u, 16V | 1812 SMD | 445-1443-1-ND | Digi-Key |
| 5 | C2, C4, C7, CR10 | Capacitors | 1u, 16V | 0603 SMD | PCC2224CT | Digi-Key |
| 6 | C5, C6, C13 | Capacitors | 2.2u, 100V | 1812 SMD | 445-1439-1-ND | Digi-Key |
| 7 | C3 | Capacitors | $4.7 \mathrm{u}, 16 \mathrm{~V}$ | 0805 SMD | PCC2323CT | Digi-Key |
| 8 | D6, D10 | Diode Zener | 5 V | SOD323 | BZT52C5V1SDICT | Digi-Key |
| 9 | D7 D8 | Diode Zener | 9.1V | SOD324 | BZT52C9V1SDICT | Digi-Key |
| 10 | D3, D4, D5, D9 | Diode Switch | 75V | SOD-123 | 1NN4148WDICT | Digi-Key |
| 11 | D1, D2 | Diode Schottky | BAT54S | SOT-23 | BAT54S | Digi-Key |
| 12 | R3 | Resistor | 3.48 | 0603 SMD | RK73H1J3R48F | Garrett |
| 13 | $\begin{gathered} \hline \text { R5, R6, R7, R8, } \\ \text { R13 } \\ \hline \end{gathered}$ | Resistor | 10K 1\% | 0603 SMD | RK73H1JLTD1002F | Garrett |
| 14 | D(R14) | Zener Diode | 12 V | SOD323 | BZT52C12SDICT | Digi-Key |
| 15 | R12 | Resistor | 20K 1\% | 0603 SMD | RK73H1JLTD2002F | Garrett |
| 16 | R9 | Resistor | 39K 1\% | 0805 SMD | 9C06031A3922FKRFT | Garrett |
| 17 | R4 | Resistor | 1.8K 1\% | 0603 SMD | 9C06031A1821FKHFT | Garrett |
| 18 | R15 | Resistor | 82K 1\% | 0603 SMD | CRCW0603-8252FRT1 | Garrett |
| 19 | R1 | Resistor | 100 1\% | 0805 SMD | RK73H2ALTD1000F T | Garrett |
| 20 | R2 | Resistor | 120K 1\% | 0603 SMD | CRCW0603-1213FRT1 | Garrett |
| 21 | R16 | Resistor | 910K 1\% | 0402 SMD | RK73H1JLTD9093F | Garrett |
| 22 | T1 | Transformer | CURRENT_SENSE | SMD | PCD1548CT-ND | Digi-Key |
| 23 | U1 | IC | IR2086 | SOIC-16 | IR2086 | IR |
| 24 | Q1, Q2, Q3, Q4 | D/FET | IRF6646 | MN | IRF6646 | IR |
| 25 | Q6, Q7, Q8, Q9 | D/FET | IRF6635 | MX | IRF6635 | IR |
| 26 | Q10, Q11 | D/FET | IRF6621 | SQ | IRF6621 | IR |
| 27 | Q5 | SO8 | IRF7380 | SO-8 | IRF7380 | IR |
| 28 | L1 | Inductor | Inductor | PLANAR_IND BRIDGE | E14/3.5/5-3F3-A160 | Elna |
| 29 | U2 | IC Volt detector | TC54 | SOT23 | TC54VN2702ECB71CT | Digi-Key |
| 30 | T2 | Planar Transformer | Planar Transformer | GAP=16Mil | TP4AEQP25/23 Plate | MH\&W |
|  |  |  |  |  | TP4AEQP25/23 Plate TP4AHEQ25/8-Z | MH\&W |
|  |  |  |  |  | 8mil Cirlex kapton | CIRLEX |
| 31 | Vin -/ I Out - | Mil Max Pin | Pins for Input and output Connection | PIN | 3125-2-00-01-00-00-08-0 | MIL MAX |
| 32 | Vin +/ I Out + | Jack | Banana Jack Black | Nylon Banana Jack | J152-ND | Digi-Key |
| 33 | Vin +/ I Out + | Jack | Banana Jack Red | Nylon Banana Jack | J151-ND | Digi-Key |

